



**Bellcomm**

955 L'Enfant Plaza North, S.W.  
Washington, D. C. 20024

date: September 24, 1971

to: Distribution

from: T. H. Crowe

subject: Effect of Operating M509 and T020 on the  
Cluster Atmosphere - Case 620

B71 09020

ABSTRACT

The problem of maintaining the cluster atmosphere within specification limits while operating Experiment M509 is discussed. Operation of M509 will cause the total pressure of the atmosphere and the partial pressure of  $O_2$  to fall outside specification limits unless some control of the atmosphere is done manually.

(NASA-CR-123238) EFFECT OF OPERATING M509  
AND T020 ON THE CLUSTER ATMOSPHERE  
(Bellcomm, Inc.) 9 p

N79-72420

Unclas  
12131

00/18

FF No. 6021	(PAGES)	(CODE)
	CR-123238	
	(NASA CR OR TMX OR AD NUMBER)	(CATEGORY)
	RESEARCH CENTERS ONLY	





**Bellcomm**

955 L'Enfant Plaza North, S.W.  
Washington, D. C. 20024

date: September 24, 1971  
to: Distribution  
from: T. H. Crowe  
subject: Effect of Operating M509 and T020 on the Cluster  
Atmosphere - Case 620

B71 09020

MEMORANDUM FOR FILE

The purpose of this paper is to discuss the problem of maintaining cluster atmosphere control while operating Experiments M509 and T020 and some of the alternatives being considered to solve the problem.

Description of the System

Figure 1 is a schematic of the atmosphere control system. Six O<sub>2</sub> tanks and six N<sub>2</sub> tanks filled to 3000 psi provide the source of gases for the atmosphere. These tanks provide 4930 lbs. of usable O<sub>2</sub> and 1320 lbs. of usable N<sub>2</sub>. The requirements, assuming specification leak rates, are 4140 lbs. and 924 lbs. of O<sub>2</sub> and N<sub>2</sub>, respectively.

The six O<sub>2</sub> tanks are manifolded and O<sub>2</sub> is routed to redundant 120 psi pressure regulators and from there to various parts of the cluster including the O<sub>2</sub> N<sub>2</sub> two-gas control system. Four of the N<sub>2</sub> tanks are manifolded and N<sub>2</sub> is routed to redundant 150 psi regulator valves and from there to various parts of the cluster including the O<sub>2</sub> N<sub>2</sub> two-gas control system. The remaining pair of N<sub>2</sub> tanks can either be isolated to provide topping off of the M509 and T020 N<sub>2</sub> bottles or can be valved into the N<sub>2</sub> manifold.

The O<sub>2</sub> N<sub>2</sub> two-gas control system consists of three O<sub>2</sub> partial pressure sensors, a solenoid controlled N<sub>2</sub> flow valve, redundant cabin pressure regulators and control electronics. Any one of the three O<sub>2</sub> partial pressure sensors



can be used for one or both functions of providing the signal to control the  $N_2$  flow valve or providing the signal for the TM system. Provision is also made for flowing pure  $O_2$  or  $N_2$  across the sensors for calibration. The control electronics associated with the  $O_2$  partial pressure sensors are set at a nominal 3.7 psia with a dead band of  $\pm 1$  psia. However, available data indicate that the normal operating range is 3.58 psia to 3.85 psia. Thus, if the output of the  $O_2$  partial pressure sensor reading is 3.85 psia or higher the  $N_2$  flow valve is opened. This closes the  $O_2$  check valves and  $N_2$  is supplied to the cabin pressure regulators. If the reading is 3.58 psia or less, the  $N_2$  flow valve is closed and  $O_2$  is supplied to the cabin pressure regulators. The accuracy of the sensors and associated electronics and the system response are not well known at this time but is thought to be such that  $O_2$  partial pressure can barely be maintained within specification limits,  $3.7 \pm 0.2$  psia.

The cabin pressure regulators maintain the total pressure at a nominal 5 psia  $\pm 0.2$  psia. The regulators are of the demand type and will attempt to flow gas at the rate it is used. The flow characteristics of the regulators are given in Figure 2.

The system is also connected into the caution and warning system so that an alarm is initiated if the  $O_2$  partial pressure drops below a nominal 3.05 psia, the total pressure drops to a range of 4.5 to 4.7 psia or if the total pressure is decaying at a rate in excess of 0.1 psi/min.

The cluster is also equipped with vent valves that crack open if the total pressure exceeds 5.5 psia and will open fully to prevent the total pressure from exceeding 6 psia.

Using specification values for leak rate the total demand for gases under normal operation is about 23.5 lbs. per day. This consists of six lbs. of  $O_2$  for metabolic use, 14 lbs  $O_2$  and  $N_2$  for leakage and 3.5 lbs.  $O_2$  and  $N_2$  for operation of the molecular sieves.



### Operation of the System

If one assumes that the cluster has been pressurized, normally done by ground command, that the switches are positioned for normal automatic control of the atmosphere, that leakage rate is at specification value and that the initial  $O_2$  partial pressure is 3.7 psia and the initial total pressure is 4.9 psia. The operation of the system is as follows.

At the nominal leakage rate the cabin pressure regulators are flowing either  $O_2$  or  $N_2$  at the rate of about .98 lbs. per hour. To initialize the system one must assume which gas is flowing. If one assumes that  $O_2$  is flowing then this continues until the  $O_2$  partial pressure reaches 3.85 psia, then  $N_2$  flows until the partial pressure of  $O_2$  reaches 3.58 psia. An approximation of the cyclic operation of the system is illustrated in Figure 3.

### M509 and T020

M509 and T020 are both astronaut maneuvering experiments utilizing gaseous  $N_2$  as propellant. Current planning for accomplishment of the objectives of the experiment are to conduct four runs for M509 during the SL-1/2 mission, one of which is in a pressurized space suit, and eight runs on the SL-3 mission, two of which are in a pressurized space suit. Four T020 runs are scheduled for SL-3, two of which are in a pressurized suit. Runs last for about one hour, and during each M509 run about 20 lbs. of  $N_2$  is released into the cabin. About 10 lbs. of  $N_2$  is released during T020 run. In addition during suited runs, about 12.3 lbs. of  $O_2$  is released into the cabin. M509 runs are currently scheduled on days 4, 8, 16, and 20 of the SL-1/2 mission and on days 8, 13, 17, 22, 25, 31, 35, and 41 of the SL-3 mission. T020 is scheduled for days 45, 48, 51, and 54 of the SL-3 mission. An approximation of the effect of these runs on cabin atmosphere pressure for the SL-1/2 mission is illustrated in Figure 4.

Several observations can be made from this figure. The  $O_2$  partial pressure varies from 3.4 psia to 3.98 psia, considerably outside the specification limits. This does not take into account the inaccuracies of the  $O_2$  partial pressure



sensors. The total pressure varies from 4.89 psia to 5.5 psia, resulting in the vent valves opening once. Similar results are obtained when one calculates the pressure profiles for the SL-3 mission.

Another way to get a feel for the problem is to look at  $N_2$  requirements. At specification leak rate the total  $N_2$  makeup requirement for the SL-1/2 mission is 116 lbs.; four runs of M509 introduce 80 lbs. of  $N_2$  into the atmosphere.

MSC has done a series of studies on the problem and determined that lower leak rates make the problem worse and that with a leak rate of about 125% the problem is all but eliminated. In order to eliminate the problem with a 50% leak rate they consider the following steps necessary.

1. Initialize the cabin pressure at  $O_2$  partial pressure 3.9 psia and  $N_2$  partial pressure 1.1 psia.
2. Inhibit automatic  $N_2$  makeup for entire mission.
3. Reschedule the experiment runs at longer time intervals, including some runs on SL-4.
4. Shutoff all makeup gases approximately 18 hours before suited runs, or manually vent the cabin atmosphere just before suited runs.

The problem is being worked by the Flight Operations Planning group and alternative solutions will probably be forwarded for management consideration within two or three months.

1025-THC-pal

  
T. H. Crowe

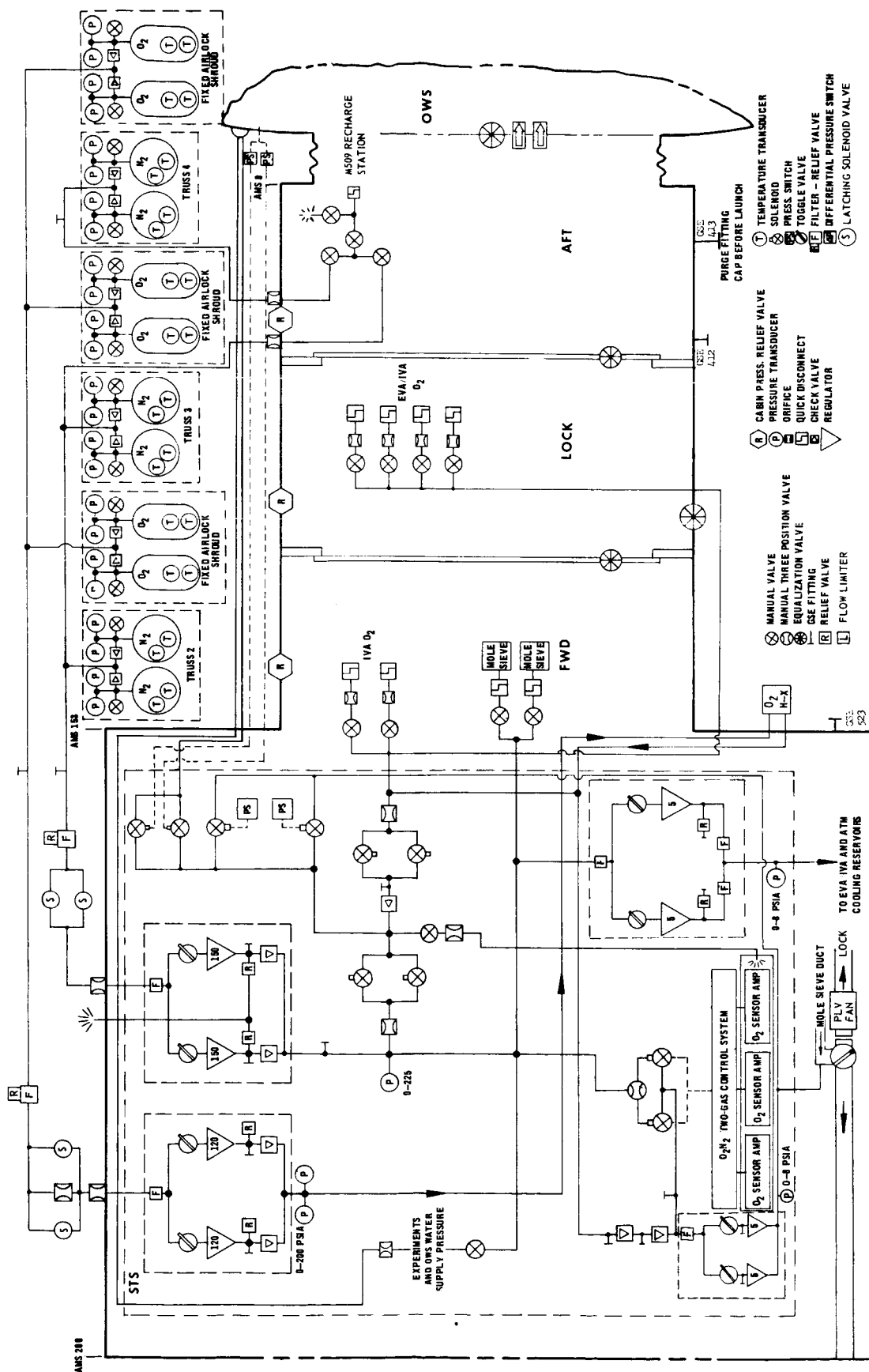


FIGURE 1 - GAS SYSTEM

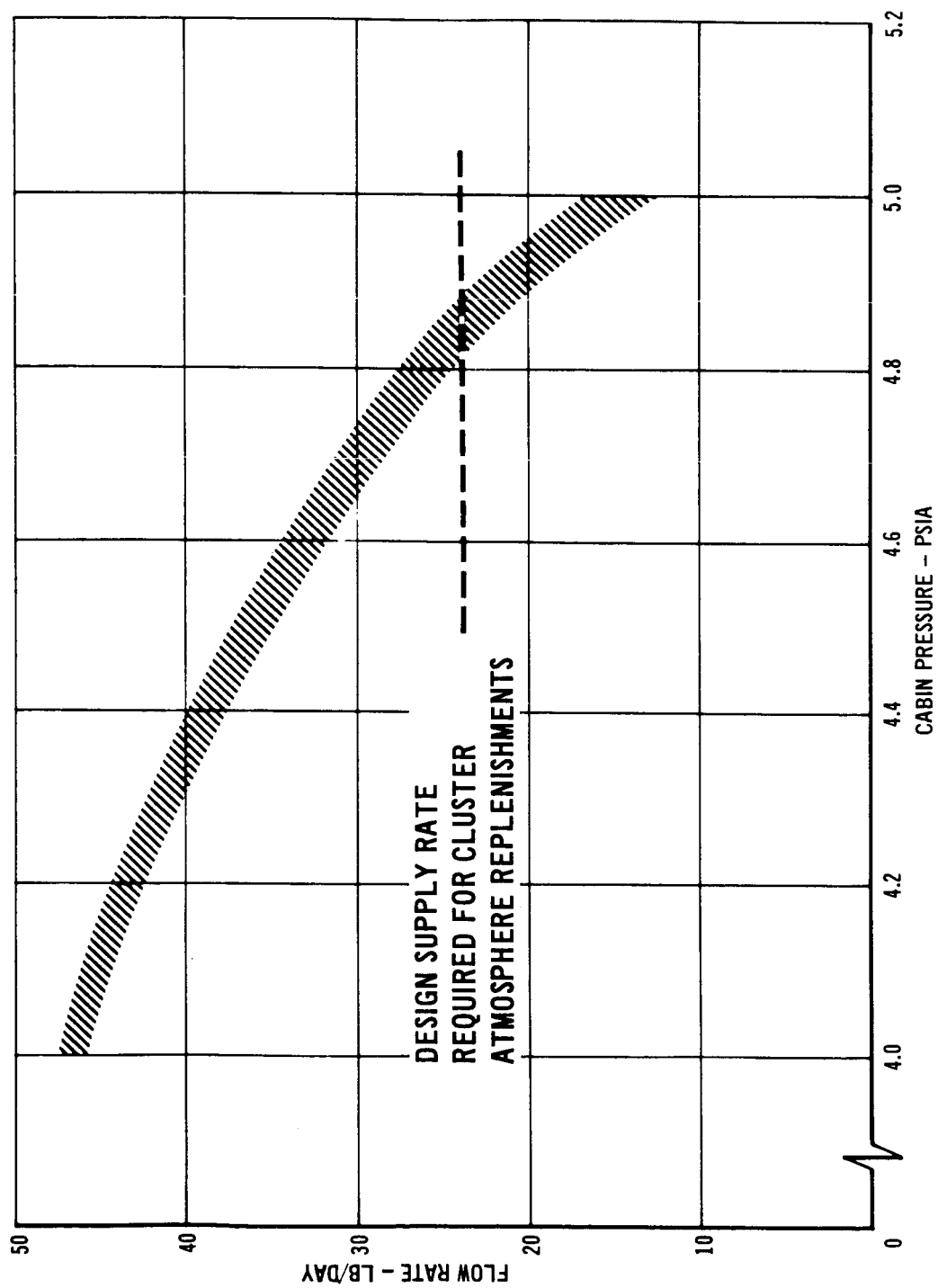


FIGURE 2 - CABIN PRESSURE REGULATOR FLOW RATE CHARACTERISTICS

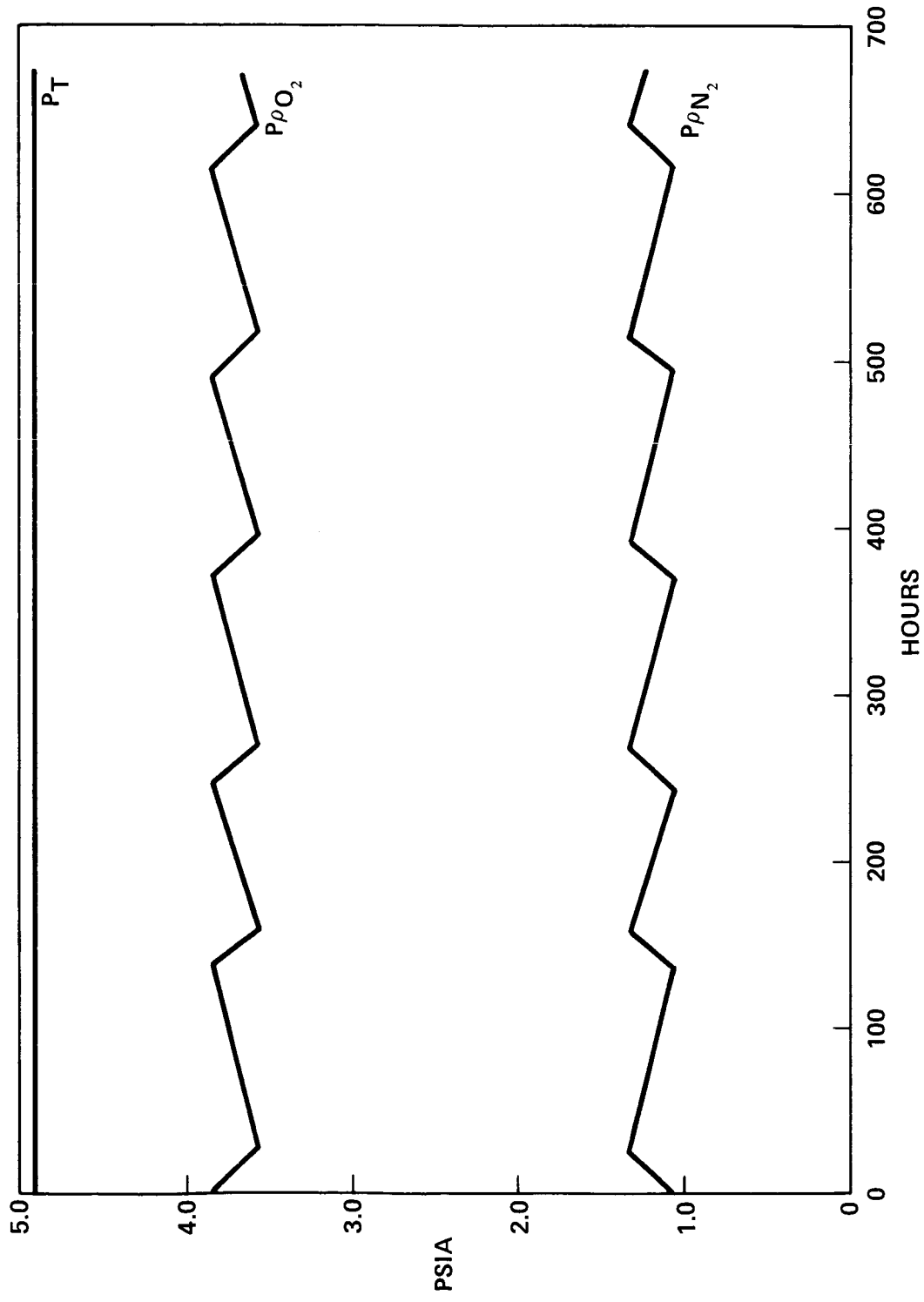


FIGURE 3 - CABIN PRESSURE - 100% LEAK RATE



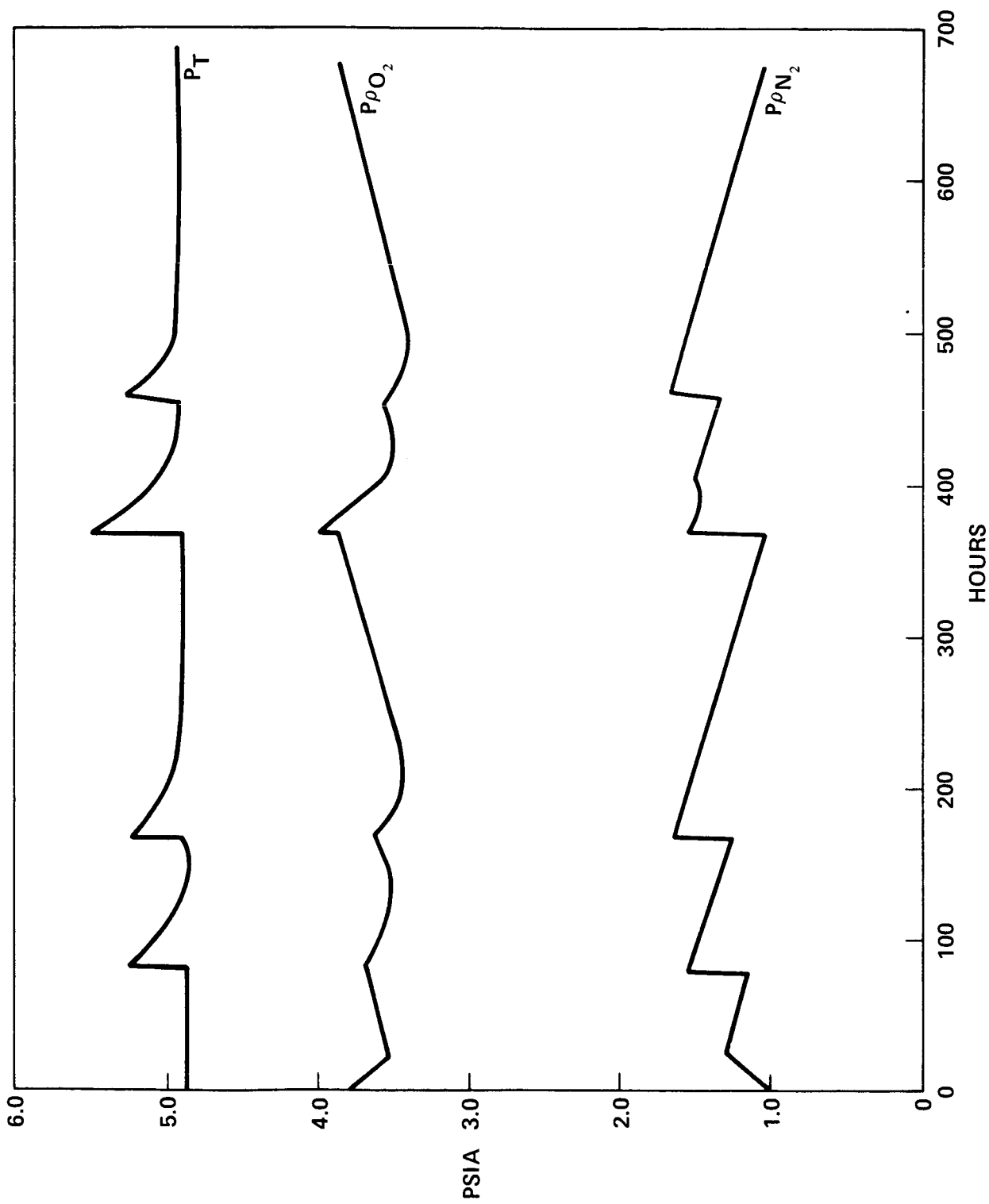


FIGURE 4 - SL1/2 CABIN PRESSURE - 100% LEAK RATE  
OPERATING M509